

Reply:

Liao, Wang, and Yang (Letter to the Editor, July 2007, pp. 1898–1899, DOI 10.1002/aic.11192) have correctly pointed out that the total regeneration targets ($F_{ws} = F_{reg} = 37.5$ t/h and $F_{ww} = 17.5$ t/h) for the water network discussed in Example 1 by Agrawal and Shenoy¹ are feasible, based on the observations of Mann and Liu² for some special multipinch cases. What must be recognized in such cases is that the regeneration inlet concentration C_{in} can be greater than the pinch concentration C_p (rather than assume $C_{in} = C_p$).

Agrawal and Shenoy¹ setup a system of three equations (Eqs. 2, 8 and 9) for the case of a single pinch point (denoted by subscript P). For the case of two pinch points (denoted by subscripts P and A), the following additional equation (which is a mass balance over the region below pinch point A) needs to be considered

$$m_A = F_{ws}(C_{in} - C_{ws}) + F_{reg}(C_A - C_o)$$

where m_A and C_A are the cumulative mass load and the concentration, respectively, of the pinch point A on the limiting composite. The above equation along with Eqs. 2, 8 and 9 constitutes a system of four equations in five unknowns (F_{ws} , F_{ww} , F_{reg} , C_{ws} , and C_{in}). Since there is one degree of freedom, we specify $F_{ws} = F_{reg}$ for the case of total regeneration, and then use the equations to determine the targets as illustrated below.

For Example 1 of Agrawal and Shenoy¹ with total regeneration, Eq. 8 on substituting $C_o = 20$ ppm, $C_p = 150$ ppm, and $m_p = 10.5$ kg/h gives the freshwater ($C_{ws} = 0$) and regeneration targets, as $F_{ws} = F_{reg} = m_p / (2C_p - C_{ws} - C_o) = 37.5$ t/h. Then, Eq. 2 with $\Delta_1 = 20$ t/h gives $F_{ww} = 17.5$ t/h. Now, the new equation given above with $C_A = 250$ ppm and $m_A = 15$ kg/h yields $C_{in} = m_A / F_{ws} + C_{ws} + C_o - C_A = 170$ ppm (which is higher than $C_p = 150$ ppm). Finally, Eq. 9 with $\Delta_2 = -10$ kg/h gives $C_{ww} = 250$ ppm.

The targets of 37.5 t/h (for freshwater), 17.5 t/h (for wastewater) and 37.5 t/h (for regeneration) for Example 1 with total regeneration may be achieved in practice through many different network designs. Several networks, all of which feature minimum freshwater consumption, may be designed using the *nearest neighbors algorithm* (NNA)³ depending on the order in which the demands are satisfied. Figure 1

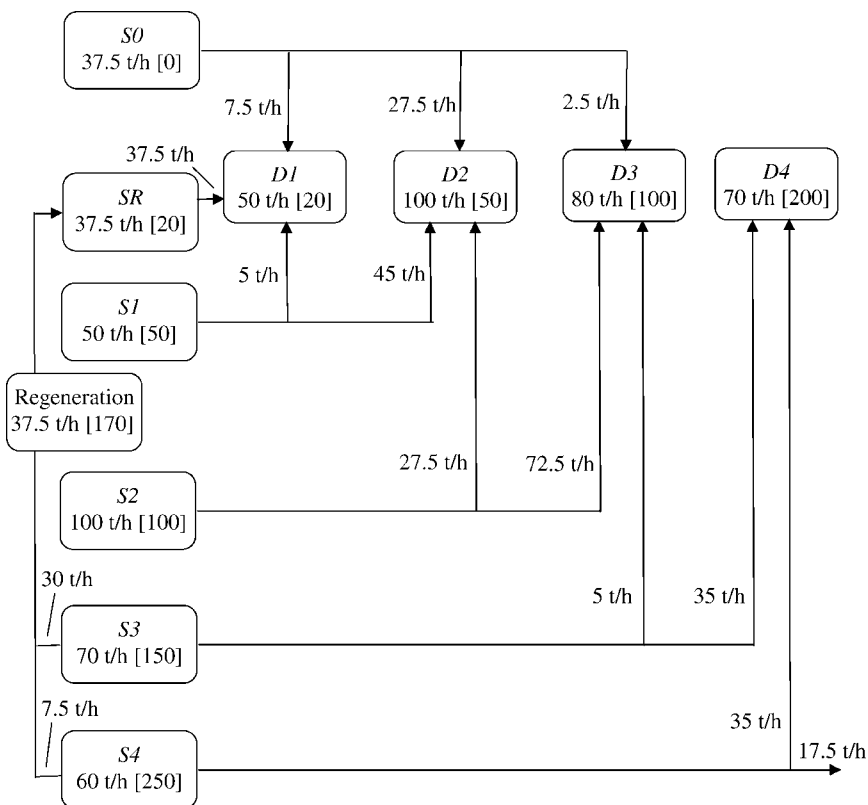


Figure 1. Network for Example 1 by NNA for total regeneration.

Labels show contaminant concentrations [ppm] and flow rates (t/h).

shows a possible network obtained by a straightforward application of the NNA (starting with demand $D1$, and then satisfying demands $D2$, $D3$, and $D4$ in that order). The regenerated water provides an additional source SR of 37.5 t/h at 20 ppm, which is entirely used to satisfy the demand $D1$ (also at 20 ppm). The source SR is itself obtained by regenerating water from sources $S3$ (30 t/h) and $S4$ (7.5 t/h) at $C_{in} = 170$ ppm.

In summary, it may be noted that targets and networks for minimum freshwater may be obtained for total regeneration, provided the regeneration inlet concentration is at or above the pinch concentration ($C_{in} \geq C_p$). To determine C_{in} , a supplementary equation corresponding to the mass balance over the region below the additional pinch must be considered.

Literature Cited

1. Agrawal V, Shenoy UV. Unified conceptual approach to targeting and design of water and hydrogen networks. *AIChE J.* 2006;52(3): 1071–1082.
2. Mann JG, Liu YA. Industrial water reuse and wastewater minimization. McGraw-Hill; 1999.
3. Prakash R, Shenoy UV. Targeting and design of water networks for fixed flowrate and fixed contaminant load operations. *Chem Eng Sci.* 2005;60:255–268.

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